TEMPERATURE DEPENDENCE SIMULATION OF THE EMISSION COEFFICIENT VIA EMITTER CAPACITANCE

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ABSTRACT

The need to increase accuracy and stability in the design of temperature sensors and bandgap references has lead to recent experimental studies of the emission coefficient n. In particular an unexplained increase of n at low temperatures has been measured in CMOS vertical bipolar pnp transistors. In this paper a new procedure for the simulation of n is presented using Gummel-Poon's expression of n as a function of Ce, and HICUM's compact model expression of Ce as a function of temperature. This new procedure allows a physical approach to explain temperature dependence of n. Simulation results show that the temperature dependence parameter η of V_{BE} plays a major role in the increase of n at low temperatures.

RESUMEN

La necesidad de aumentar la exactitud y la estabilidad en el diseño de los sensores de temperatura y las referencias de bandgap han dado lugar a estudios experimentales del coeficiente de emisión n. En particular un incremento no explicado de n a bajas temperaturas ha sido medido en transistores bipolares verticales pnp en tecnología CMOS. En este artículo se presenta un nuevo procedimiento para la simulación de n utilizando la expresion de Gummel-Poon para n en función de Ce y la expresión de Ce del modelo compacto HICUM en función de la temperatura. Este nuevo procedimiento enfoca la dependencia de n con la temperatura desde un punto de vista físico. Los resultados de simulación muestran que el parámetro η de la dependencia con la temperatura de V_{BE} , juega un papel importante en el aumento de n a bajas temperaturas.

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ABSTRACT

An unexpected increase of the emission coefficient n of bipolar transistors at low temperature and constant bias current has been experimentally shown recently. In this paper an increase of n at low temperatures is shown in the simulation of a typical bipolar transistor for high values of parameter η and at certain bias current levels. The emission coefficient has been calculated using Gummel-Poon's expression as a function of Ce, and HICUM's compact model expression of Ce as a function of temperature.

1. INTRODUCTION

The need to increase accuracy and stability in the design of temperature sensors and bandgap references has lead to recent experimental studies [1] on the variation with temperature of the emission coefficient n at constant bias current. In particular an unexplained increase of n at low temperatures has been measured in CMOS vertical bipolar pnp transistors.

Many authors [2,3] consider the emission coefficient as in the SPICE-Gummel-Poon model (SGP)[4], with a constant value close to unity to explain the non ideality of the exponential dependence of collector current I_C on emitter base voltage, $I_C \alpha \exp(qV_{be}/nkT)$.

Nevertheless in the original Gummel-Poon model (GP) [5] n is not a parameter and it is defined, at given V_{cb} and T, as the reciprocal of the slope of the Gummel plot. It can be shown that at low level injection n depends on the emitter capacitance and is given by [5], $n \approx 1 + kTC_e/qQ_{b0}$. Because Ce increases significantly under forward bias conditions [6], n should also increase.

The SGP model cannot simulate this behavior because of the constant C_e assumption in its DC model. This assumption was made [7] to obtain a constant output conductance similar to that of the Ebers-Moll model, because at that time the original GP model was not universally accepted.

In this paper a new simulation procedure is presented to obtain the emission coefficient of a bipolar transistor biased at constant collector current. This procedure uses the original Gummel-Poon's expressions [5] as a function of C_e , and HICUM's compact model expressions of C_e as a function of temperature [8]. In this simulation Gummel-Poon's sample transistor [5] is used because the values of its 21 parameters at 300 K are known. At other temperatures the Gummel-Poon model is not adequate [4].

2. THE EMISSION COEFFICIENT

The emission coefficient is defined [5] as the reciprocal of the slope of the Gummel plot ($\ln I_C$ vs $qV_{be'}kT$) and is given by the analytical expression,

$$\frac{1}{n} = \frac{kT}{qI_C} \frac{dI_C}{dV_{eb}}\Big|_{V_{cb}=constant}$$
(1)

The emision coefficient n is not a parameter in the original Gummel-Poon model as can be seen from the collector current expression,

$$I_{C} = -I_{S}Q_{b0} \frac{\exp\left(\frac{qV_{eb}}{kT}\right) - \exp\left(\frac{qV_{cb}}{kT}\right)}{Q_{b}} + I_{bc} \qquad (2)$$

In expression (2) Q_{b0} , the zero-bias charge in the base, can be considered constant and Q_b , the "base charge", includes besides Q_{b0} , capacitive and current charge contributions that depend on junction voltages taking care of the non ideal behavior of ln $I_{\rm C}$ vs $qV_{\rm be}/kT$ at low and high level injection.

At low level injection and zero biased collector junction, $Q_b = Q_{b0} + Q_e$, and if $Q_{b0} >> Q_e$, n is given by [5],

$$n \approx 1 + \frac{kTC_e}{qQ_{b0}}$$
(3)

where $C_e = \frac{dQ_e}{dV_{eb}}\Big|_{V_{cb}=constant}$ is the emitter capacitance.

3.MODELING EMITTER CAPACITANCE

From expression (3), to simulate n with temperature, adequate modeling of Ce is required. Because GP model is not adequate for temperature variation [4], HICUM's compact model expression [8] for emitter capacitance is used.

Emitter capacitance in HICUM model is also based on clasical depletion capacitance expression,

$$C_{je} = \frac{C_{je0}}{\left(1 - \frac{V_{BE}}{V_{DE}}\right)^{Z}}$$
(4)

whose three parameters are,

V_{DE}: diffusion or built-in voltage

C_{je0}: zero bias emitter capacitance

z: grading coefficient

Under significant forward bias, emitter capacitance increases to a maximum value that can not be explained with expression (4) and in HICUM compact model it has been modified with a four parameters expression that also includes a smoothing function,

$$C_{je} = \frac{C_{je0}}{(1 - V_j / V_{DE})^z} \frac{e}{1 + e} + a_{je} C_{je0} \frac{1}{1 + e}$$
(5)

where \mathbf{e} , \mathbf{V}_{j} , \mathbf{V}_{f} and the fourth parameter \mathbf{a}_{je} are given by the expressions,

$$e = \exp\left(\frac{V_j - V_{be}}{V_T}\right)$$
(6)

$$\mathbf{V}_{j} = \mathbf{V}_{f} - \mathbf{V}_{T} \ln(1 + \mathbf{e}) \tag{7}$$

$$V_{f} = V_{DE} \left[1 - a_{je}^{-(1/z)} \right]$$
 (8)

$$a_{je} = \frac{C_{jemax}}{C_{je0}}$$
(9)

Temperature dependence in this model is given by expressions,

$$C_{je0}(T) = C_{je0}(T_r) \left(\frac{V_{DE}(T_r)}{V_{DE}(T)} \right)^{z}$$
(10)

$$a_{je}(T) = a_{je}(T_r) \frac{V_{DE}(T)}{V_{DE}(T_r)}$$
 (11)

The key parameter for temperature dependence of capacitance is the diffusion (or built-in) voltage V_{DE} given in HICUM model by ,

$$V_{DE}(T) = V_{G0} \left(1 - \frac{T}{T_r} \right) + V_{DE}(T_r) \frac{T}{T_r} - 3V_T \ln \left(\frac{T}{T_r} \right)$$
(12)

To model $V_{BE}(T)$, instead of HICUM model, the bandgap linear approximation is used, which based on experimentally measured parameters η and V_{G0} , is very accurate [9,10],

$$V_{BE}(T) = V_{G0} \left(1 - \frac{T}{T_r} \right) + V_{BE}(T_r) \frac{T}{T_r} - \eta V_T \ln \left(\frac{T}{T_r} \right)$$
(13)

where T_r is the reference temperature considered here 300 K. The GP model is not used because it is not adequate for temperature variations [4], and HICUM's V_{BE} model does not consider parameters η and V_{G0} that depend on base impurity concentration [10].

4.SIMULATION OF N WITH GUMMEL-POON'S SAMPLE TRANSISTOR

The simulation of n with temperature uses GP's sample transistor [5] because it is well characterized by the values of its 21 parameters at 300 K [5]. The transistor is biased here at constant collector current.

This simulation is performed in the 240 to 300 K interval using expressions (3) and (5) to (13). The values of Ce parameters of HICUM model $C_{je0}(T_r) = 1.51$ pF, $a_{je}(T_r) = 5.735$, z = 0.48, $V_{DE}(T_r) = 0.700535$ V, are obtained from the values $v_{oe} = 27.1$, $m_e = 0.24$, $a_{e1} = 0.337$ and $a_{e2} = 1.03 \times 10^{-2}$, of sample transistor.

The value of Q_{b0} calculated from Q_{b0} =-I_k τ_f [5] is 6.0 pC and its temperature dependence is considered negligible [8].

To simulate the temperature behavior of the base- emitter voltage using expression (13) it is necessary to know the values of η , V_{G0} and $V_{BE}(T_r)$. The value of $V_{BE}(T_r)$ is obtained solving the full set of GP's equations [5]. Because η and V_{G0} are not part of GP's model, their values are taken from experimental measurements of transistors in two different technologies: npn transistors of

a standard IC bipolar technology [9] and pnp vertical substrate bipolar transistors in a CMOS technology [11]. Two levels of bias current are considered: 100 μ A and 200 μ A, which are not high considering that the knee current I_K of sample transistor is 18.75 mA.

5. SIMULATION RESULTS

The values $\eta = 3.618$ and $V_{G0} = 1.1707$ V characterize temperature dependence of $V_{BE}(T)$ in npn transistors of a standard bipolar IC process [9].

Simulation is performed at $I_C=100\mu A$ and $I_C=200\mu A$ with corresponding values $V_{BE}(T_r)=0.612265$ V and $V_{BE}(T_r)=0.630702$ V of the sample transistor.

The simulation results are shown in Fig. 1. The emission coefficient shows a decrease at low temperatures.



Fig. 1 Emission coefficient temperature dependence of sample transistor with η =3.618, V_{G0}=1.1707 V at two bias current levels.

In vertical ppp transistors of a CMOS technology [11] η shows high values with a spread between 4.8 and 5.2.

With a selected value of η =5.1, V_{G0} =1.12046 V was calculated from the linear regression equation [11] between η and V_{G0} .



Fig. 2 Emission coefficient temperature dependence of sample transistor with η =5.1, V_{G0}=1.12046 V at two bias current levels

Simulation in this case shows in Fig. 2. an increase of n at low temperature. It can be noticed that at the higher bias current the increase of n is slightly greater.

6. DISCUSSION AND CONCLUSIONS

Simulation results show that for higher values of η , the emission coefficient n increases at low temperatures. This can be explained considering the ideal depletion emitter capacitance expression (4). From this expression, if V_{BE} approaches V_{DE} at lower temperatures, C_e will increase rapidly with the possibility to overcome the decrease of T in expression (3) of the emission coefficient.

From expressions (13) and (12) of $V_{BE}(T)$ and $V_{DE}(T)$ it can be seen that at low temperatures, where T< T_r, all terms in both equations are positive, and $V_{BE}(T)$ will approach $V_{DE}(T)$ as temperature decreases, only if $\eta > 3$.

Generally the emission coefficient is obtained from the slope of a Gummel plot.

In this paper the expression (3) of Gummel-Poon is used because in relating n with the emitter capacitance Ce, it allows a physical approach of its behavior with forward bias and temperature which has been widely studied regarding Ce [12,5,6,8].

The use of the expression of n as a function of Ce allows also to see that the constant Ce assumption in the SPICE-Gummel-Poon model is inadequate to characterize n. This constant Ce assumption has also been reported as a limitation to represent the output conductance g_0 [7].

7. REFERENCES

- [1]G.Wang,G.C.M.Meijer,The temperature characteristics of bipolar transistors fabricated in CMOS technology, Sensors and Actuators, 87 (2000) 81-89.
- [2]Y.P. Tsividis, Accurate analysis of the temperature effects in I_C – V_{BE} characteristics with application to bandgap reference sources, IEEE J. Solid-State Circuits, 15 (1980) 1076-1084.
- [3]T.Quarles et al, SPICE3 Version 3F5 User's Manual, University of California, Berkeley, 1994 pp.33-34.
- [4] Ian E Getreu, Modeling the bipolar transistor, Elsevier, 1978 pp. 116-123.
- [5] H.K Gummel, H. C.Poon, An integral charge control model of bipolar transitors, BSTJ, May-June (1970) 827-852.
- [6]B.C. Bouma, A.C. Roelofs, An experimental determination of the forward-bias emitter-base capacitance,
- Solid-State Electronics, 21 (1978) 833-836.
 [7] Colin C. McAndrew, L.W. Nagel, Early effect modelling in SPICE, IEEE Journal of Solid State Circuits, 31(1996) 136-138.
- [8] M. Schroter, HICUM, A scalable physics-based compact bipolar transistor model, available on the web:

http://www.iee.et.tu-dresden.de/iee/eb/comp_mod.html

- [9] G.C.M. Meijer, Integrated circuits and components for bandgap references and temperature transducers, Ph.D. thesis, Delft University of Technology, The Netherlands, Appendix B, 1982 pp. 61-62.
- [10] R. Amador, A. Polanco, A. Nagy, The spread of η and V_{G0} and its influence on the sensitivity of a bipolar IC Celsius sensor, Sensors and Actuators, 77 (1999) 9-13.
- [11] G. Wang, G.C.M. Meijer, The temperature characteristics of bipolar transistors for CMOS temperature sensors, 13 th European Conference on Solid-State Transducers, The Hague, Netherlands, Sept. 12 15 1999, pp. 553- 556.
- [12]H.C. Poon, H.K, Gummel, Modeling of emitter capacitance, Proc. IEEE, Dec. (1969) 2181-2182.
- [13] B.R. Chawla, H.K. Gummel, An experimental determination of the forward-biased emitter-base capacitance, IEEE Trans. Electron Devices, 18 (1971) 178.